



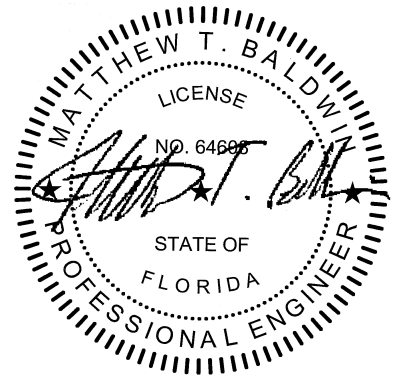
ENGINEERING STRUCTURAL WIND CALCULATIONS For Gillette 100-400KW 132" Frame Genset

July 14, 2016

132" LG Frame Genset Models:

PR-1000	SP-2000	SPMD-2500	SPVD-2500	T4D-1000
PR-1300		SPMD-2800	SPVD-3000	T4D-1500
PR-1800		SPMD-3000	SPVD-3500	T4D-2000
			SPVD-4000	

Designed with reference from: 2014 Florida Building Code
ASCE 7 - Minimum Design Loads for Buildings and Other Structures
2005 Aluminum Association Design Manual
ANSI/AISC 360-05 Specifications for Structural Steel Buildings



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Project Information

Project Name/Model # - Gillette 100-400KW 132" Frame Genset
Project Number -
 Project Description - 180mph Windload Calculations
 Project Location -
 Customer -
 Mounting Location - Ground

Enclosure Materials

Roof Beam - 0.062 Aluminum Truss - 5052-H34
 Roof Panels - 0.080 Aluminum Panel - 5052-H34
 Wall Panels - 0.080 Aluminum Panel - 5052-H34

Components

GenSet Manufacturer - Gillette Generators, Inc.
 GenSet Size and Model - 100-400 KW - 132" Frame
 Base - Bent Steel Frame

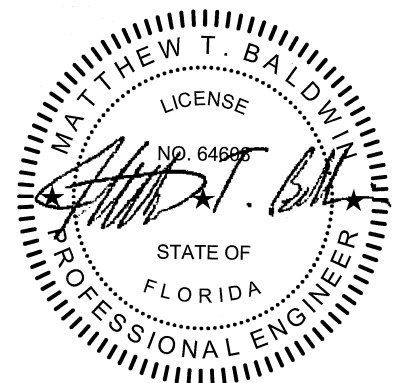
Supported by - Base

Fasteners/Hardware

	Bolt Size	Grade/Finish
Panels	5/16" - 18	Grade 18-8/SS
Enclosure to Base	5/16" - 18	Grade 18-8/SS

Specification Requirements

Wind Speed - 180 mph (Greater of Design or Site)
 Exposure Category - D



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Enclosure Dimensions & Component Weights

Gillette 100-400KW 132" Frame Genset

Roof Style- Flat

Enclosure Dimensions (ft)

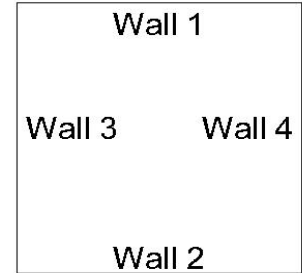
Wall	Length (ft)		Height (ft)
1	4.33	x	6.021
2	4.33	x	6.021
3	14.5	x	6.021
4	14.5	x	6.021

Base Dimensions

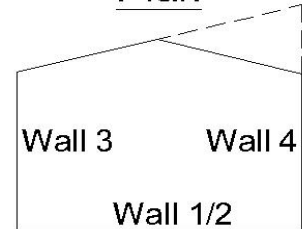
Width (Wall 1/2 Side)	=	52	in
Length (Wall 3/4 Side)	=	132	in
Height	=	8	in

Roof/Eave Information

Roof Pitch Angle - (θ)	=	0.0	Degrees
Eave/Roof Height - h	=	6.021	



Plan



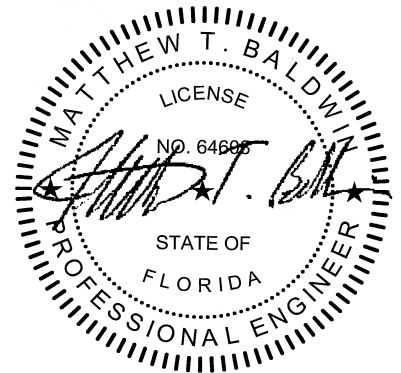
Elevation

Structure Areas

Walls 1/2 Area - $(w1)$	=	26.1	ft ²	=	3,754	in ²
Walls 3/4 Area - $(w3)$	=	87.3	ft ²	=	12,572	in ²
Roof Area - (R)	=	62.8	ft ²	=	9,041	in ²
Base Side 1/2	$(T1)$	=	416.0	in ²		
Base Side 3/4	$(T3)$	=	1,056.0	in ²		

Component Weights

Genset	=	4,765	lbs
Enclosure	=	1,270	lbs
Base Frame	=	400	lbs



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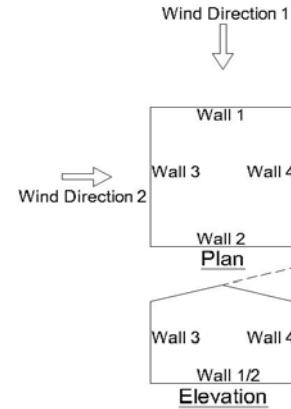
MWFRS Net Pressures

Gillette 100-400KW 132" Frame Genset

Wind

Directional Procedure method from ASCE 7 are utilized in these calculations.

Enclosure Classification	-	Enclosed
Exposure Category	-	D
Basic Wind Speed	(V)	180 mph
Wind Directionality Factors	(K _d)	0.85
Internal Pressure Coefficients	(GC _{pi})	± 0.18
Velocity Pressure Exposure Coefficient	(K _z)	1.03
Roof Mean Height Above Ground Level	(z)	6.69 ft
Velocity Pressure	(q)	72.63 psf



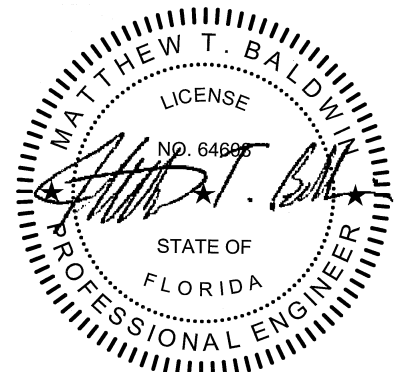
Wind Direction 1

	Enclosure								
	Wall #			Roof					
	1	2	3&4	Parallel to Ridge				(C _p)2	
				(C _p)1 (Distance From Windward Edge)					
	Windward	Leeward	Side	0 to 3.0	3.0 to 6.0	6.0 to 12.0	> 12.0		
Background Response Factor (Q)	0.97	0.97	0.96	0.97					
Gust Effect Factors (G)	0.91	0.91	0.91	0.91					
External Pressure Coefficients (C _p)	0.80	-0.233	-0.70	-0.90	-0.90	-0.50	-0.3	-0.18	
Net Pressures with + (GC _{pi}) - psf (Net _{p+})	39.9	-28.5	-59.1	-72.7	-72.7	-46.2	-33.0	-25.0	
Net Pressures with - (GC _{pi}) - psf (Net _{p-})	66.1	-2.3	-33.0	-46.6	-46.6	-20.1	-6.8	1.1	

Wind Direction 2

	Enclosure								
	Wall #			Roof - Normal To Ridge					
	3	4	1&2	(C _p)1 (Distance From Windward Edge)				(C _p)2	
				0 to 3.0	> 3.0				
	Windward	Leeward	Side						
Background Response Factor (Q)	0.96	0.96	0.97	0.96					
Gust Effect Factors (G)	0.91	0.91	0.91	0.91					
External Pressure Coefficients (C _p)	0.80	-0.5	-0.70	-1.04	-0.70			-0.18	
Net Pressures with + (GC _{pi}) - psf (Net _{p+})	39.6	-46.0	-59.5	-81.5	-59.1			-24.9	
Net Pressures with - (GC _{pi}) - psf (Net _{p-})	65.7	-19.8	-33.3	-55.4	-33.0			1.2	

Plus and minus signs signify pressures acting toward or away from the surfaces, respectively.



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Structural Calculations - Roof

Gillette 100-400KW 132" Frame Genset

Critical Loads & Pressures

Wind Pressures

Downforce 1.228 psf = 0.01 psi

Uplift -81.52 psf = -0.57 psi

Section Properties

0.062 Aluminum Truss - 5052-H34

Cross Sectional Area (A) = 0.30 in²
Moment of Inertia - x (I_x) = 0.27 in⁴
Moment of Inertia - y (I_y) = N/A in⁴
Section Modulus - x (S_x) = 0.31 in³
Section Modulus - y (S_y) = N/A in³
Radius of Gyration - x (r_x) = 0.94 in
Radius of Gyration - y (r_y) = N/A in
Polar Moment of Inertia (J) = N/A in⁴
Weight of Beam (w) = 0.03 lbs/in
Modulus of Elasticity (E) = 1.02E+04 ksi
Safety Factor (n_u) = 1.95
Safety Factor (n_y) = 1.65
Coefficient (k_t) = 1.00
Tensile Ultimate Strength (F_{tu}) = 34 ksi
Tensile Yield Strength (F_{ty}) = 26 ksi
Compressive Yield Strength (F_{cy}) = 24 ksi
Shear Ultimate Strength (F_{su}) = 20 ksi

Roof Frame Calculations

Member Designed for Forces Acting on the [Strong Axis](#)

Interior Beam Critical Member Dimensions

Interior Beam Length (L_i) = 42.81 in

Load Spanned Width (W_i) = 36.19 in

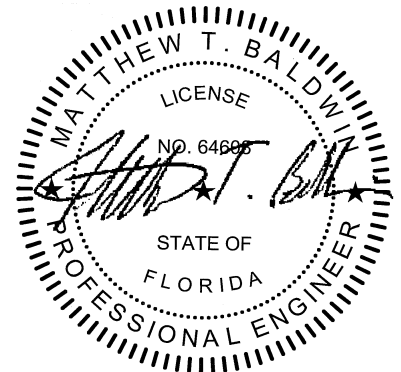
Interior Beam Calculated Forces

Distributed Loads

Weight of Beam (w) = 0.029 lbs/in

Wind Load Downforce (w_d) = 0.309 lbs/in

Wind Load Uplift Force (w_u) = -20.486 lbs/in



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Shear Forces (Maximum at End)

Beam Weight Shear $(V_b) = 0.63$ lbs
 Wind DownForce Shear $(V_{wd}) = 6.6$ lbs
 Wind Uplift Shear $(V_{wu}) = -438.5$ lbs

Total Shear Downward = 7.2 lbs
 Total Shear Upward = 437.9 lbs

Design Shear $(V_{bi}) = \underline{437.9}$ lbs

Stress Forces (Bending)

Beam Weight Moment $(M_b) = 4$ lb-in
 Wind Downforce Moment $(M_d) = 35$ lb-in
 Wind Uplift Moment $(M_u) = -2,347$ lb-in

Total Moments Downward = 40 lb-in
 Total Moments Upward = 2,342 lb-in

Design Moment $(M_T) = 2,342$ lb-in

Design Stress $(\sigma_{bi}) = \underline{7,590}$ psi

Interior Beam Design Calculations

Allowable Shear Strength

Slenderness Limit 1 $(S_1) = 28.54$
 Slenderness Limit 2 $(S_2) = 102.40$
 Slenderness Ratio $(S) = 18.0$

Allowable Shear Stress = 9,098 psi
 Allowable Shear Strength $(V_n) = 2,758$ lbs

Conclusion

(V_{bi}) 438 lbs < (V_n) 2,758 lbs **OK**

Allowable Stresses For Tension And Compression (Bending)

Tension

Allowable Tensile Stress $(F_t) = 16,000$ psi

Compression

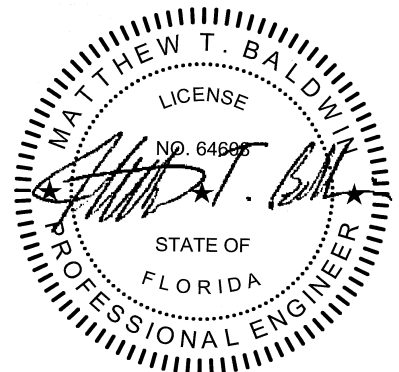
Slenderness Limit 1 $(S_1) = 25.0$
 Slenderness Limit 2 $(S_2) = 125.0$
 Slenderness Ratio $(S) = 45.5$

Allowable Compressive Stress $(F_c) = 12,755$ psi

The Allowable Compressive Stress is the controlling failure design strength.
Therefore, $(F_b) = \underline{12,755}$ psi

Conclusion

(σ_{bi}) 7,590 psi < (F_b) 12,755 psi **OK**



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Entire Roof Uplift Calculations

Roof Area

$$\text{Area of Roof Subjected to Uplift } (R) = 9,041 \text{ in}^2$$

Roof Uplift Calculated Forces

To be conservative, the weight of the roof frame and panels is neglected.

$$\text{Weight of Accessories } (\omega_a) = 0 \text{ lbs}$$

$$\text{Wind Load Uplift Force } (W_{ru}) = -5,118 \text{ lbs}$$

$$\text{Total Roof Design Uplift } (W_{ru}) = \underline{-3,071} \text{ lbs}$$

Mounting Hardware - Roof Frame to Wall Panels

$$\text{Screws Along Length - 1 Side} = 10 \quad 5/16" - 18 \quad - \text{ Grade 18-8/SS}$$

$$\text{Screws Along Width - 1 Side} = 3 \quad 5/16" - 18 \quad - \text{ Grade 18-8/SS}$$

$$\text{Total Mounting Screws} = 26 \quad 5/16" - 18 \quad - \text{ Grade 18-8/SS}$$

Entire Roof Uplift Design Calculations

$$\text{Grade 18-8 Ultimate Strength} = 150,000 \text{ psi}$$

$$\text{5/16 Bolt Nominal Diameter} = 0.255 \text{ in}$$

$$\text{5/16 Bolt Effective Area} = 0.051 \text{ in}^2$$

$$\text{5/16 SBolt Threads per Inch} = 18$$

$$\text{Washer Nominal Diameter} = 0.875 \text{ in}$$

$$\text{Wall Panel Tensile Ult. Strength} = 34 \text{ ksi}$$

$$\text{Wall Panel Tensile Yield Strength} = 26 \text{ ksi}$$

$$\text{Safety Factor} = 3$$

$$\text{Wall Panel Nominal Thickness} = 0.080 \text{ in}$$

$$\text{Maximum Tensile Strength} = 566.7 \text{ lbs}$$

$$\text{Maximum Shear/Bearing Strength} = 408.6 \text{ lbs}$$

$$\text{Max. Tensile Load per Screw} = 408.6 \text{ lbs}$$

$$\text{Max. Total Screws Tensile Strength } (P_{ts}) = \underline{10,623} \text{ lbs}$$

Conclusion

$$(W_{ru}) \quad 3,071 \quad \text{lbs} < (P_{ts}) \quad 10,623 \quad \text{lbs} \quad \text{OK}$$

Roof Panel Uplift Calculations

Roof Panel Critical Member Dimensions

$$\text{Critical Panel Length } (L_p) = 73.38 \text{ in}$$

$$\text{Critical Panel Width } (W_p) = 52 \text{ in}$$

Roof Panel Uplift Calculated Forces

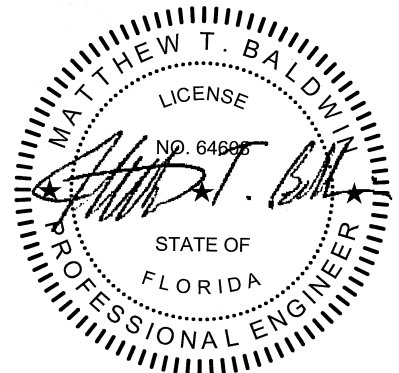
Distributed Loads

$$\text{Wind Load Uplift Force } (W_{pu}) = \underline{1,296.0} \text{ lbs}$$

Mounting Hardware - Roof Panel to Roof Frame

$$\text{Screws Along Length - 1 Side} = 3 \quad 5/16" - 18 \quad - \text{ Grade 18-8/SS}$$

$$\text{Screws Along Width - 1 Side} = 3 \quad 5/16" - 18 \quad - \text{ Grade 18-8/SS}$$



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Roof Panel Uplift Design Calculations

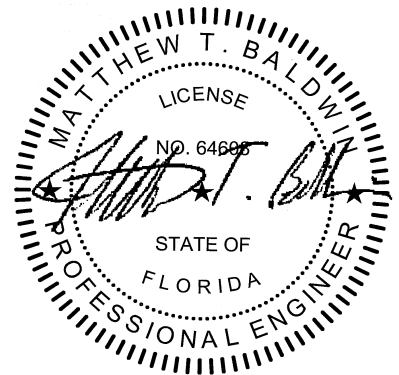
Grade 410 Ultimate Strength = 150,000 psi
5/16 Bolt Nominal Diameter = 0.255 in
5/16 Bolt Effective Area = 0.051 in²
5/16 Bolt Threads per Inch = 18
Washer Nominal Diameter = 0.875 in
Roof Panel Tensile Ult. Strength = 34 ksi
Roof Panel Tensile Yield Strength = 26 ksi
Safety Factor = 3
Roof Panel Nominal Thickness = 0.080 in

	Roof Frame		
Maximum Tensile Strength	= 566.7	lbs	(Accounts for screw pull-over strength)
Maximum Shear/Bearing Strength	= 408.6	lbs	
Max. Tensile Load per Screw	= 408.6	lbs	

Max. Total Screws Tensile Strength (P_{ts}) = 4,903 lbs

Conclusion

(w_{pu}) 1,296 lbs < (P_{ts}) 4,903 lbs **OK**



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Structural Calculations - Walls/Columns

Gillette 100-400KW 132" Frame Genset

Critical Wind Load Pressures and Roof Forces

Walls 1 & 2

Maximum Pressures Acting:

$$\begin{aligned} \text{Toward} & 66.1 \text{ psf} = 0.4590 \text{ psi} \\ \text{Away} & -59.5 \text{ psf} = -0.4130 \text{ psi} \end{aligned}$$

Walls 3 & 4

Maximum Pressures Acting:

$$\begin{aligned} \text{Toward} & 65.7 \text{ psf} = 0.4564 \text{ psi} \\ \text{Away} & -59.1 \text{ psf} = -0.4107 \text{ psi} \end{aligned}$$

Critical Wall Panel Dimensions

$$\begin{aligned} \text{Critical/Maximum Panel Width} & = 52 \text{ in} \\ \text{Critical/Maximum Panel Height} & = 72.0 \text{ in} \end{aligned}$$

Section Properties

0.080 Aluminum Panel - 5052-H34

$$\begin{aligned} \text{Cross Sectional Area} & (A) = 4.11 \text{ in}^2 \\ \text{Moment of Inertia - x} & (I_x) = 0.05 \text{ in}^4 \\ \text{Section Modulus - x} & (S_x) = 0.83 \text{ in}^3 \\ \text{Radius of Gyration - x} & (r_x) = 0.11 \text{ in} \\ \text{Modulus of Elasticity} & (E) = 1.02\text{E}+04 \text{ ksi} \\ \text{Safety Factor} & (n_u) = 1.95 \\ \text{Factor of Safety} & (n_y) = 1.65 \\ \text{Coefficient - Tension Member} & (k_t) = 1.0 \\ \text{Tensile Ultimate Strength} & (F_{tu}) = 34 \text{ ksi} \\ \text{Tensile Yield Strength} & (F_{ty}) = 26 \text{ ksi} \\ \text{Shear Ultimate Strength} & (F_{su}) = 20 \text{ ksi} \\ \text{Compressive Yield Strength} & (F_{cy}) = 24 \text{ ksi} \end{aligned}$$

Critical Wall Panel Calculated Forces

Maximum Wind Pressure on Walls

$$\begin{aligned} \text{Maximum + Wind Pressure} & = 0.4590 \text{ psi} \\ \text{Maximum - Wind Pressure} & = -0.4130 \text{ psi} \end{aligned}$$

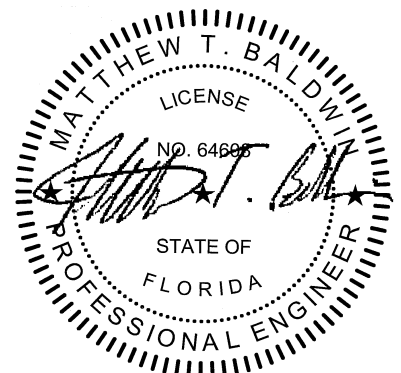
Plus and minus signs signify pressures acting toward or away from the surfaces, respectively.

Wind Shear Distributed Loads on Critical Panel

$$\begin{aligned} \text{Maximum + Wind Shear} & = 23.9 \text{ lbs/in} \\ \text{Maximum - Wind Shear} & = -21.5 \text{ lbs/in} \end{aligned}$$

Total Wind Shear on Critical Panel

$$\text{Total Panel Design Shear } (V_{ww}) = 1,718.4 \text{ lbs}$$



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Critical Panel Roof Load (Roof to Wall)

Axial Roof Load $(W_{wr}) = 0.0$ lbs

Mounting Hardware - Wall Panel to Wall Panel

To be conservative, the 'wall to roof' and 'wall to floor' connections are neglected.

Bolts Along Length - 1 Side = 4 5/16" - 18 - Grade 18-8/SS

Total Mounting Screws = 8 5/16" - 18 - Grade 18-8/SS

Wall Panel Design Calculations

Mounting Hardware - Shear and Tension

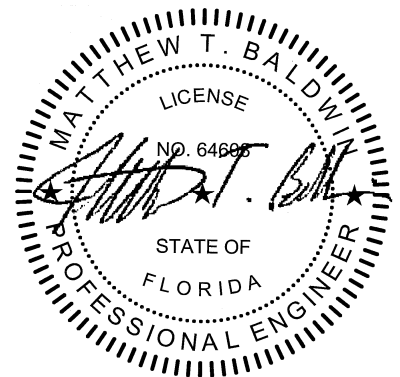
Grade 18-8/SS = 150,000 psi
Grade 18-8/SS Shear Strength = 30,000 psi (Includes Reduction Factor)
Grade 18-8/SS Tensile Strength = 57,000 psi (Includes Reduction Factor)
5/16" Bolt Effective Area = 0.0510 in²
Shear Strength per Bolt = 1,530 lbs
Tensile Strength per Bolt = 2,907 lbs

Total Bolts Shear Strength $(R_{vb}) = 12,240$ lbs

Total Bolts Tensile Strength $(R_{tb}) = 23,256$ lbs

Conclusion

(V_{ww}) 1,718 lbs < (R_{vb}) 12,240 lbs **OK**



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Structural Calculations - Enclosure to Base/Tank or Pad

Gillette 100-400KW 132" Frame Genset

Critical Pressures & Loads

To determine maximum moment forces, pressures are algebraically combined relative to toward or away forces (+ & -) and each wind direction.

Wind Direction 1

Net Pressures with + Internal Pressure(+Gcpi)

Walls 1 & 2	-	68.4	psf =	0.4752	psi
Wall 3 or 4	-	59.1	psf =	0.4107	psi
Roof Uplift	-	72.7	psf =	0.5050	psi

Net Pressures with - Internal Pressure(-Gcpi)

Walls 1 & 2	-	68.4	psf =	0.4752	psi
Wall 3 or 4	-	33.0	psf =	0.2291	psi
Roof Uplift	-	46.6	psf =	0.3234	psi

Wind Direction 2

Net Pressures with + Internal Pressure(+Gcpi)

Walls 3 & 4	-	85.6	psf =	0.5941	psi
Wall 1 or 2	-	59.5	psf =	0.4130	psi
Roof Uplift	-	81.5	psf =	0.5661	psi

Net Pressures with - Internal Pressure(-Gcpi)

Walls 3 & 4	-	85.6	psf =	0.5941	psi
Wall 1 or 2	-	33.3	psf =	0.2314	psi
Roof Uplift	-	55.4	psf =	0.3845	psi

Enclosure Critical Dimensions & Weights

Total Enclosure Weight	(W_t) =	1,270	lbs
Walls 1/2 Area	-	($w1$) =	3754.2 in ²
Walls 3/4 Area	-	($w3$) =	12571.8 in ²
Roof Area	-	(R) =	9041.0 in ²

(Includes all components)

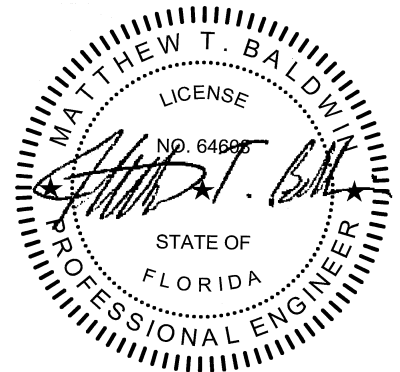
Enclosure Calculated Forces

Maximum Wind Load Forces on Walls

Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Walls 1/2	-	=	1,784	lbs
Wall 3 or 4	-	=	5,163	lbs
Roof Uplift	-	=	4,566	lbs



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Net Forces with - Internal Pressure(-Gcpi)

Walls 1/2	-	=	1,784	lbs
Wall 3 or 4	-	=	2,880	lbs
Roof Uplift	-	=	2,924	lbs

Wind Direction 2

Net Forces with + Internal Pressure(+Gcpi)

Walls 3/4	-	=	7,469	lbs
Wall 1 or 2	-	=	1,550	lbs
Roof Uplift	-	=	5,118	lbs

Net Forces with - Internal Pressure(-Gcpi)

Walls 3/4	-	=	7,469	lbs
Wall 1 or 2	-	=	869	lbs
Roof Uplift	-	=	3,476	lbs

Enclosure Overturn Forces

(Positive forces act upward, negative forces act downward)

Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 1/2	=	322	lbs
Overturn on Walls 3/4	=	2,254	lbs

Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 1/2	=	-171	lbs
Overturn on Walls 3/4	=	809	lbs

Wind Direction 2

Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 3/4	=	3,381	lbs
Overturn on Walls 1/2	=	1,094	lbs

Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 3/4	=	2,889	lbs
Overturn on Walls 1/2	=	-119	lbs

Design Overturn Force (O_E) = 3,381 lbs Acting On Wall 3/4

Mounting Hardware - Enclosure to Base/Tank or Pad

To be conservative, half the bolt connections along the adjacent walls are neglected.

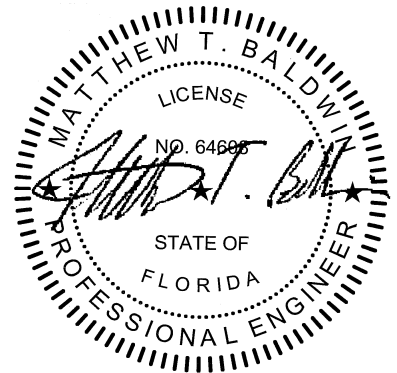
No. of Bolt Connections Along Wall 3/4 = 8 5/16" - 18 - Grade 18-8/SS

Enclosure Overturn Design Calculations

Grade 18-8 Ultimate Strength	=	150,000	psi
Grade 18-8 Shear Strength	=	30,000	psi (Includes Reduction Factor)
5/16" Bolt Effective Area	=	0.051	in ²
Shear Strength per Bolt	=	1,530	lbs
Total Bolts Shear Strength	(R_{vb}) =	12,240	lbs

Conclusion

(O_E) 3,381 lbs < (R_v) 12,240 lbs **OK**



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