

# ENGINEERING STRUCTURAL CALCULATIONS For Gillette 68" Frame Gensets

March 12, 2025

Models SP-250, SPD-300

Location: Florida

Designed in compliance with: 2023 Florida Building Code, 8th Edition ASCE 7 - 22 Minimum Design Loads for Buildings and Other Structures 2020 Aluminum Association Design Manual ANSI/AISC 360-22 - Specification for Structural Steel Buildings

Anchoring: 1/2" Bolt/Anchors - Minimum (2) per side (4) total

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# **Project Information**

# Project Name/Model #

- Gillette 68" Frame Gensets
- **Project Number Project Description Project Location** Customer Mounting Location
- Sound Attenuated Generator Enclosure
- Florida
- Ground

# **Enclosure Materials**

- **Roof Panels** Wall Panels Base Frame/Skid
- 0.080 Aluminum Panel 5052-H34
- 0.060 Aluminum Panel 5052-H34
- Aluminum Formed Steel 'C' Channel

# **Components**

GenSet Manufacturer GenSet Size and Model Base

- Gillette
- SP-250, SPD-300
- Aluminum Formed Steel 'C' Channel
- Supported by -Base

# Fasteners/Hardware

			Bolt Size	Washer	Nut	Grade/Finish
Roof to Walls Wall to Wall Walls to Base Base to Slab/Tank	- - -	5 5 5 1/2"	/16" - 18 Bolts /16" - 18 Bolts /16" - 18 Bolts Set Bolt Anchors	5/16" Washer 5/16" Washer 5/16" Washer Flat Washers	Nut Clip Nut Clip Nut Clip Hex Nuts	Grade 18-8/SS Grade 18-8/SS Grade 18-8/SS Grade 5/Galv.
Specification Require	ments				THE WILL	N. T. B. A. L. D. CENSE P. 64600
Wind Speed Exposure Category	-	200 D	mph		ST PROS	
Risk Category Ground Snow Load ( $P_g$ Fig Ice Thickness ( $t$ Fig 10-2 to1 and Concurrent Wind Gust ( Seizmin Site Class	- 7.1) - 0-6) - (V <sub>c</sub> )-	III 0 0.25 30	psf in mph		Matthe	WALENGINI

# Enclosure Dimensions & Component Weights

# **Gillette 68" Frame Gensets**

## Roof Style- Flat

## **Enclosure Dimensions (ft)**

<u>Wall</u>	Length (ft)		<u>Height (ft)</u>
1	3	х	3.65
2	3	х	3.65
3	6.84	х	3.65
4	6.84	х	3.65

## **Base Dimensions**

Width (Wall 1/2 Side)	=	36	in
Length (Wall 3/4 Side)	=	68	in
Height	=	4	in

# **Roof/Eave Information**

Roof Pitch Angle -	<i>(θ)</i> =	0.0	Degrees
Eave/Roof Height -	h =	3.983	-



# **Structure Areas**

Walls 1/2 Area	-	(w1) =	12.0	$ft^2 = ft^2 = $	1,721	in²
Walls 3/4 Area	-	(w3) =	27.2		3,923	in²
Roof Area	-	(R) =	20.5		2,955	in²
Base Side 1/2 Base Side 3/4		(T1) = (T3) =	144.0 272.0	in2 in2		

## Component Weights (lightest setup for worst case)

Genset	=	0	lbs	(Varies, so will use zero to be conservative/most uplift to resist)	
Enclosure	=	283	lbs	(Based on Aluminum to be conserative/most uplift to resist)	
Base	=	273	lbs	(Based on Aluminum to be conserative/most uplift to resist)	LICENSE

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# **MWFRS Net Pressures**

# **Gillette 68" Frame Gensets**

## **Wind**

Analytical Procedure method and Load Combinations from ASCE 7 are utilized in these calculations.

Enclosure Classification	-	Enclosed	ł
Exposure Category	-	D	
Basic Wind Speed	(V)	200	mph
Importance Factor (Wind)	$(I_w)$	1.15	
Wind Directionality Factors	(K <sub>d</sub> )	0.85	
Internal Pressure Coefficients	(GC <sub>pi</sub> )	± 0.18	
Velocity Pressure Exposure Coefficient	$(K_z)$	1.03	
Roof Mean Height Above Ground Level	(Z)	4.32	ft
Velocity Pressure	(q)	103.12	psf

## Wind Direction 1

				Enclos	ure				
			Wall #				Roof		
		1	2	384	Parallel to Ridge				
		1		2	304	(C <sub>p</sub> )1	(Distance Fi	rom Windward	Edge)
		Windward	Leeward	Side	0 to 2.0	2.0 to 4.0	4.0 to 6.8		( <i>Op</i> )2
Background Response Factor	(Q)	0.98	0.98	0.97			0.98		
Gust Effect Factors	(G)	0.92	0.92	0.91			0.92		
External Pressure Coefficients	(C <sub>p</sub> )	0.80	-0.286	-0.70	-0.92	-0.87	-0.53		-0.18
Net Pressures with + (GC pi) - psf	(Net <sub>p+</sub> )	56.9	-45.6	-84.4	-105.7	-100.4	-68.9		-35.5
Net Pressures with - (GC <sub>pi</sub> ) - psf	(Net <sub>p-</sub> )	94.1	-8.4	-47.3	-68.5	-63.3	-31.7		1.6

# Wind Direction 2

		Enclosure								
			Wall #			Roo	f - Norma	al To R	lidge	
		3	3 1							
		5	4	102	(C <sub>p</sub> )1	(Distance From Windward Edge)		d Edge)	$(C_{1})^{2}$	
		Windward	Leeward	eward Side	0 to 2.0	> 2.0			$(O_p)^2$	
Background Response Factor	(Q)	0.97	0.97	0.98	0.97					
Gust Effect Factors	(G)	0.91	0.91	0.92			0.9	1		
External Pressure Coefficients	(C <sub>p</sub> )	0.80	-0.5	-0.70	-1.04	-0.70			-0.18	
Net Pressures with + $(GC_{pi})$ - psf	(Net <sub>p+</sub> )	56.7	-65.6	-84.6	-116.4	-84.4			-35.5	
Net Pressures with - (GC <sub>pi</sub> ) - psf	(Net <sub>p-</sub> )	93.8	-28.5	-47.5	-79.3	-47.3			1.6	

Plus and minus signs signify pressures acting toward or away from the surfaces, respectively.

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Elevation

Wind Direction 1 Υ.

## <u>Snow</u>

Importance Factor (Snow) Exposure Factor	(1 <sub>s</sub> ) (C <sub>a</sub> )	1.1 0.8		
Thermal Factor	$(C_{t})$	1.2		
Slope Factor	$(C_s)$	1.0		
Flat Roof Snow Load	(p <sub>s</sub> )	0	psf	
<u>Seismic</u>				
Importance Factor (Seismic)	(I <sub>sm</sub> )	1.25		
Mapped Acceleration Parameter	(S <sub>s</sub> )	0.14	Figures	22-1 Thru 22-14
Mapped Acceleration Parameter	(S1)	0.07	Figures	22-1 Thru 22-14
Site Coefficient	(F <sub>a</sub> )	1	-	
Site Coefficient	$(F_v)$	1		
MCE Spectral Resp. Accel. Short Per.	$(S_{MS})$	0.140		
MCE Spectral Resp. Accel. 1-s Period	(S <sub>M1</sub> )	0.07		
Design Spectral Accel. Short Period	$(S_{DS})$	0.093		
Design Spectral Accel. 1-s Period	$(S_{D1})$	0.04667		
Fundamental Period of Structure	$(T_a)$	0.053	sec	
Long Period Transistion Period	$(T_L)$	8	sec	Figure 22-15 Thru 22-20
Seismic Design Category	-	Α		
Total Effective Seismic Weight	$(W_{eff})$	609	lbs	

Response Modification Coeficien	t	(R)	2	Table 12.2-1
System Overstrength Factor		$(\Omega_{o})$	2.5	Table 12.2-1
Deflection Amplification Factor		(C <sub>d</sub> )	2	Table 12.2-1
Seismic Response Coefficient		(C <sub>s</sub> )	0.058	
Resultant Seismic Forces				
Horizontal Seismic Load Effect	-	$(E_h)$		
Force at Base of Base	=	0.0	kips	
Force at Top of Base	=	0.0	kips	

=

0

kips

Vertical Seismic Load Effect ( $E_v$ ) =

Force on Silencer

Force at Top/Bottom of Enclosure = 0.003 kips

(Factor, Used With Deadweight in Load Combinations) 0



# **Structural Calculations - Roof**

# **Gillette 68" Frame Gensets**

## **Critical Loads & Pressures**

-116.4 psf

### **Wind Pressures**

#### Downforce 1.632 psf = 0.01 psi

= -0.81 psi

# Snow Pressure

0.000

psi

psf =

0

## Seismic Load

Horizontal Vertical Factor

3 lbs 0

=

=

**Roof Live Load** 

Uplift

Downforce 20.0 psf 0.1389 = psi or 300 lbs Concentrated Load

Pressures & loads are the numerical maximums to be analyzed for shear, bending tension, and compression.

## **Section Properties**

0.080 Aluminum Panel - 5052-H34

Modulus of Elasticity	(E)	=	1.02E+	04	ksi	
Safety Factor	(Ω)	=	1.67			
Plastic Section Mod x	$(Z_x)$	=	0.18			
Plastic Section Mod y	$(Z_y)$	=	0.18			
Tensile Ultimate Strength			(F <sub>tu</sub> )	=	34	ksi
Tensile Yield Strength			$(F_{ty})$	=	26	ksi
Compressive Yield Streng		$(F_{cy})$	=	24	ksi	
Shear Ultimate Strength			(F <sub>su</sub> )	=	20	ksi

## **Entire Roof Uplift Calculations**

## Roof Area

Area of Roof Subjected to Uplift (R) 2,955 jn<sup>2</sup> (not including discharge hood area) =

### **Roof Uplift Calculated Forces**

Roof Weight	$(\omega_a)$	=	102	lbs
Wind Load Uplift Force	(w <sub>ru</sub> )	=	-2,388	lbs

Total Roof Design Uplift  $(W_{ru}) =$ <u>-2,286</u> lbs

## Mounting Hardware - Roof Frame to Wall Panels

Screws Along Length - 1 Side	=	5	5/16" - 18 Bolts
Screws Along Width - 1 Side	=	2	5/16" - 18 Bolts
Total Mounting Screws	=	14	5/16" - 18 Bolts

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#### 5/16" - 18 Bolts Page 4 - 1

# Entire Roof Uplift Design Calculations

Grade 18-8/SS Ult. Strength 5/16" Bolt Nominal Diamete 5/16" Bolt Effective Area 5/16" Bolt Threads per Inch Washer Nominal Diameter Wall Panel Tensile Ult. Strengt Wall Panel Tensile Yield Streng Safaty Easter	n = r = = h = gth =		150,000 0.255 0.051 18 0.875 34 26 2	psi in in <sup>2</sup> in ksi ksi						
Wall Panel Nominal Thickness	=	=	0.0620	in						
Maximum Tensile Strength Maximum Shear/Bearing Stren	= ath =	=	439.2 408.6	lbs lbs						
Max. Tensile Load per Bolt	=	=	408.6	lbs						
Max. Total Screws Tensile Stre	ength		$(P_{ts}) =$	<u>5</u> ,	720	<u>lbs</u>				
Conclusion										
(W <sub>ru</sub> ) 2,286 II	os <	<	$(P_{ts})$	5,	720	lbs		<u>0K</u>		
Roof Panel Uplift Calc	ulat	ic	<u>ons</u>							
Roof Panel Critical Membe	er Dir	n	<u>ensions</u>							
Critical Panel Length (L Critical Panel Width (N	p) = /p) =	=	68.00 in 36.00 in							
Roof Panel Uplift Calculat	ed Fo	or	<u>ces</u>							
Distributed Loads										
Wind Load Uplift Force (w	<sub>pu</sub> ) =	=	<u>1,978.5</u>	lbs						
Mounting Hardware - Roof Panel	to Roc	of	<u>Frame</u>							
Screws Along Length - 1 Sid Screws Along Width - 1 Side	de = e =	=	7 3		5/16 5/16	" - 18 " - 18	8 Bolts 8 Bolts	5 ·	- Grade - Grade	18-8/SS 18-8/SS
Roof Panel Uplift Design (	Calcu	la	ations							
Grade 18-8/SS Ult. Strength 5/16" Bolt Nominal Diamete 5/16" Bolt Effective Area 5/16" Bolt Threads per Inch Washer Nominal Diameter Roof Panel Tensile Ult. Streng Roof Panel Tensile Yield Stren Safety Factor	n = r = = th = gth =		150,000 0.255 0.051 18 0.875 34 26 3	psi in in <sup>2</sup> in ksi ksi						
Roof Panel Nominal Thickness	=	=	0.0800	in						
Maximum Tanaila Strangth	_	_	Roof Frame			_	(Accou	ints for and p	screw ull-out	J)
Maximum Tensile Strength Maximum Shear/Bearing Stren	= gth =	=	439.2 408.6				strengt	ns)		
Max. Tensile Load per Scre	w =	=	408.6							
Max. Total Screws Tensile Stre	ength		$(P_{ts}) =$	<u>8,</u>	<u>.171</u>	<u>lbs</u>				PROUNT
(w <sub>pu</sub> ) 1,978 lbs <	(P <sub>ts</sub> ,	)	8,171	lbs	<u>0</u>	<u>K</u>				Motthe



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# **Structural Calculations - Wall Panel**

# **Gillette 68" Frame Gensets**

## **Critical Loads & Pressures**

### Walls 1 & 2

Maximum Pressures Acting:

Toward	94.1	psf	=	0.6532	psi
Away	-84.6	psf	=	-0.5876	psi

## Walls 3 & 4

#### Maximum Pressures Acting:

Toward	93.8	psf	=	0.6514	psi
Away	-84.4	psf	=	-0.5861	psi

#### Roof Forces on Critical Panel (From Roof Frame Calculations)

Maximum Downforce	$(W_d) =$	512	lbs
Wind Load Uplift Force	$(w_{pu}) =$	1,978	lbs

Pressures and weights are the numerical maximums to be analyzed for shear, tension, and compression.

## Critical Wall Panel Dimensions

Critical/Maximum Panel Width	=	33.50	in
Critical/Maximum Panel Height	=	42.00	in

## **Section Properties**

0.060 Aluminum Panel - 5052-H34

Cross Sectional Area	(A)	=	2.21	in <sup>2</sup>		
Moment of Inertia - x	$(I_x)$	=	0.052	in <sup>4</sup>		
Moment of Inertia - y	$(I_y)$	=	N/A	in <sup>4</sup>		
Section Modulus - x	$(S_x)$	=	0.810	in <sup>3</sup>		
Section Modulus - y	$(S_y)$	=	N/A	in <sup>3</sup>		
Radius of Gyration - x	$(r_x)$	=	0.154	in		
Radius of Gyration - y	$(r_y)$	=	N/a	in		
Weight	<i>(\mathcal{\mathcal</i>	=	0.026	lbs/	in <sup>2</sup>	
Modulus of Elasticity	(E)	=	1.02E	+04	ksi	
Safety Factor	<b>(</b> Ω)	=	1.6	7		
Plastic Section Mod x	$(Z_x)$	=	0.1	3		
Plastic Section Mod y	$(Z_{\gamma})$	=	0.1	3		
Tensile Ultimate Strength	ı <sup>´</sup>		(F <sub>tu</sub> )	=	34	ksi
Tensile Yield Strength		$(F_{tv})$	=	26	ksi	
Compressive Yield Streng		$(F_{cv})$	=	23	ksi	
Shear Ultimate Strength		(F <sub>su</sub> )	=	20	ksi	
	_					

## Wall Panel Calculations

### **Critical Wall Area**

Area of Wall Panel		(W)	=	1,407.0 in <sup>2</sup>				
Mounting Hardware - Roof Frame to Wall Panels								
Screws Along Height - 1 Side	=	3		5/16" - 18 Bolts				
Screws Along Width - 1 Side	=	6		5/16" - 18 Bolts				

Total Mounting Screws	=	18	5/16" - 18 Bolts
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Grade 5 Ultimate Strength	=	150,000	psi	
5/16" Bolt Nominal Diameter	=	0.255	in	
5/16" Bolt Effective Area	=	0.051	in <sup>2</sup>	
5/16" Bolt Threads per Inch	=	18		
Washer Nominal Diameter	=	0.875	in	
Roof Panel Tensile Ult. Strength	=	34	ksi	
Roof Panel Tensile Yield Strength	=	26	ksi	
Safety Factor	=	3		
Roof Panel Nominal Thickness	=	0.0800	in	
		Roof Frame		
Maximum Tensile Strength	=	388.7		<ul> <li>(Accounts for screw pull-over and pull-out strengths)</li> </ul>
Maximum Shear/Bearing Strength	=	300.0		
Max. Tensile Load per Bolt	=	300.0		
Max. Total Screws Tensile Strengtl	<u>1</u>	$(P_{ts}) =$	<u>4,793</u>	lbs
Conclusion				

 $(w_{pu})$  919 lbs <  $(P_{ts})$  4,793 lbs <u>OK</u>



# **Structural Calculations - Enclosure to Base**

# **Gillette 68" Frame Gensets**

## **Critical Pressures & Loads**

To determine maximum moment forces, pressures are algebraically combined relative to toward or away forces (+ & -) and each wind direction.

#### Wind Direction 1

To be conservative, roof downforce is neglected.

Net Pressures with + Internal Pressure(+Gcpi)

Walls 1 & 2 -	102.5 p	sf =	0.7117	psi
Wall 3 or 4 -	84.4 p	sf =	0.5861	psi
Roof Uplift -	105.7 p	sf =	0.7338	psi

Net Pressures with - Internal Pressure(-Gcpi)

Walls 1 & 2 -	102.5	psf =	0.7117	psi
Wall 3 or 4 -	47.3	psf =	0.3283	psi
Roof Uplift -	68.5	psf =	0.4760	psi

#### Wind Direction 2

Net Pressures with + Internal Pressure(+Gcpi)

Walls 3 & 4 -	122.3	psf =	0.8491	psi
Wall 1 or 2 -	84.6	psf =	0.5876	psi
Roof Uplift -	116.4	psf =	0.8082	psi

#### Net Pressures with - Internal Pressure(-Gcpi)

Walls 3 & 4 -	122.3	psf =	0.8491	ps
Wall 1 or 2 -	47.5	psf =	0.3298	ps
Roof Uplift -	79.3	psf =	0.5504	ps

### <u>Seismic</u>

Horizontal Seismic Force  $(E_h) = 3$  lbs

### **Enclosure Critical Dimensions & Weights**

Total Enclosure	Weight	$(W_t)$	=	283	lbs
Walls 1/2 Area	-	(w1)	=	1720.8	in <sup>2</sup>
Walls 3/4 Area	-	(w3)	=	3923.4	in <sup>2</sup>
Roof Area	-	(R)	=	2954.9	in <sup>2</sup>

## **Enclosure Calculated Forces**

### Maximum Wind Load Forces on Walls

#### Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Walls 1/2 -	=	1,225	lbs
Wall 3 or 4 -	=	2,300	lbs
Roof Uplift -	=	2,168	lbs

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(Includes all components)

#### Net Forces with - Internal Pressure(-Gcpi)

Walls 1/2 -	=	1,225	lbs
Wall 3 or 4 -	=	1,288	lbs
Roof Uplift -	=	1,407	lbs

### Wind Direction 2

#### Net Forces with + Internal Pressure(+Gcpi)

Walls 3/4 -	=	3,332	lbs
Wall 1 or 2 -	=	1,011	lbs
Roof Uplift -	=	2,388	lbs

#### Net Forces with - Internal Pressure(-Gcpi)

Walls 3/4 -	=	3,332	lbs
Wall 1 or 2 -	=	568	lbs
Roof Uplift -	=	1,626	lbs

#### Enclosure Overturn Forces (Includes Seismic)

(Postive forces act upward, negative forces act downward)

#### Wind Direction 1

#### Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 1/2 Overturn on Walls 3/4	= =	1,299 2,469	lbs lbs			
Net Forces with - Internal Pre	essure(	-Gcpi)				
Overturn on Walls 1/2 Overturn on Walls 3/4	= =	918 1,417	lbs lbs			
Wind Direction 2						
Net Forces with + Internal Pre	essure	(+Gcpi)				
Overturn on Walls 3/4 Overturn on Walls 1/2	= =	3,264 1,347	lbs Ibs			
Net Forces with - Internal Pre	essure <i>(</i>	-Gcpi)				
Overturn on Walls 3/4 Overturn on Walls 1/2	= =	2,883 837	lbs lbs			
Design Overturn Force	(0 <sub>E</sub> )	= <u>3,2</u>	<u>64</u> lb	s Acting	On Wall 3/	4

#### Mounting Hardware - Enclosure to Base/Tank or Pad

To be conservative, bolt connections along the adjacent walls are neglected. No. of Bolt Connections Along Wall 3/4 = 5 5/16" - 18 Bolts - Grade 18-8/S

#### **Enclosure Overturn Design Calculations**

Grade 18-8 Ultimate Strength =	150,000	psi	
Grade 8.8 Nom. Tensile Stress =	112,500	psi	(Includes Reduction Factor)
5/16" Bolt Effective Area =	0.051	in <sup>2</sup>	
Tensile Strength per Bolt =	2,873	lbs	
Total Bolts Tensile Strength	=	14,3	64 lbs

#### **Conclusion**

 $(O_E)$  3,264 lbs <  $(R_v)$  14,364 lbs



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# Structural Calculations - Enclosure With Base/Tank to Pad

# **Gillette 68" Frame Gensets**

## **Critical Wind Load Pressures**

To determine maximum moment forces, pressures are algebraically combined relative to toward or away forces (+ & -) and each wind direction.

#### Wind Direction 1

To be conservative, roof downforce is neglected.

Net Pressures with + Internal Pressure(+Gcpi)

Walls 1 & 2 -	102.5	psf =	0.7117	psi
Wall 3 or 4 -	84.4	psf =	0.5861	ps
Roof Uplift -	105.7	psf =	0.7338	ps

#### Net Pressures with - Internal Pressure(-Gcpi)

Walls 1 & 2 -	102.5	psf =	0.7117	psi
Wall 3 or 4 -	47.3	psf =	0.3283	psi
Roof Uplift -	68.5	psf =	0.4760	psi

#### Wind Direction 2

#### Net Pressures with + Internal Pressure(+Gcpi)

Walls 3 & 4 -	122.3	psf =	0.8491	psi
Wall 1 or 2 -	84.6	psf =	0.5876	psi
Roof Uplift -	116.4	psf =	0.8082	psi

#### Net Pressures with - Internal Pressure(-Gcpi)

Walls 3 & 4 -	122.3	psf =	0.8491	psi
Wall 1 or 2 -	47.5	psf =	0.3298	psi
Roof Uplift -	79.3	psf =	0.5504	psi

#### Seismic

Enclosure Horiz. Seismic Force  $(EE_h) = 3$  Ibs Base/Tank Horiz. Seismic Force  $(EB_h) = 6$  Ibs

### Enclosure With Base/Tank Critical Dimensions & Weights

Total Enclosure	Weight	$(W_t)$	=	556	lbs	(Includes all components)
Walls 1/2 Area	-	(w1)	=	1,865	in <sup>2</sup>	(Includes Base/Tank Surface Area)
Walls 3/4 Area	-	(w3)	=	4,195	in <sup>2</sup>	(Includes Base/Tank Surface Area)
Roof Area	-	(R)	=	2,955	in <sup>2</sup>	

### Enclosure With Base/Tank Calculated Forces

#### Maximum Wind Shear Forces on Walls Including Base/Tank

#### Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Walls 1/2 -	=	:	1,327	lbs
Wall 3 or 4 -	- =	=	2,459	lbs
Roof Uplift	- =	=	2,168	lbs



Net Forces with - Internal Pressure(-Gcpi)

Walls 1/2 -	=	1,327	lbs
Wall 3 or 4 -	=	1,377	lbs
Roof Uplift -	=	1.407	lbs

#### Wind Direction 2

Net Forces with + Internal Pressure(+Gcpi)

Walls 3/4 -	=	3,562	lbs
Wall 1 or 2 -	=	1,096	lbs
Roof Uplift -	=	2,388	lbs

Net Forces with - Internal Pressure(-Gcpi)

Walls 3/4 -	=	3,562	lbs
Wall 1 or 2 -	=	615	lbs
Roof Uplift -	=	1,626	lbs

Enclosure with Base/Tank Maximum Wind Fo	rce	=	3,562	lbs Acting On Wall 3/4
Coefficient of Friction - Steel to Wet Concrete Frictional Resisting Force (Total Weight x $\mu_{s})$	$(\mu_s)$	= =	0.45 250	
Enclosure with Base/Tank Design Shear	(V <sub>EB</sub> )	=	3,312	

## Enclosure With Base/Tank Overturn Forces (Inlcudes Seismic)

Postive forces act upward

#### Wind Direction 1

#### Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 1/2	=	1,227	lbs
Overturn on Walls 3/4	=	2,580	lbs

#### Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 1/2	=	846	lbs
Overturn on Walls 3/4	=	1,421	lbs

#### Wind Direction 2

#### Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 3/4	=	3,484	lbs
Overturn on Walls 1/2	=	1,264	lbs

#### Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 3/4	=	3,103	lbs
Overturn on Walls 1/2	=	731	lbs

(O<sub>EB</sub>) = 3,484 Ibs Acting On Wall 3/4 Design Overturn Force



#### Mounting Hardware - Enclosure With Base/Tank to Pad

No. of Bolt Connections Along Wall 3/4 =	= 2	Bolts	1/2" Set Bolt Anchors	-	Grade 5/Galv
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### Enclosure With Base/Tank Design Calculations

#### Mounting Hardware - Shear and Tension

Grade 5	Ultim	ate St	ress	=	120,00	00	psi	
Grade 5	Nom. S	Shear S	Stress	=	48,000	0	psi	
Grade 5	Nom. T	ensile	Stress	=	90,000	0	psi	
1/2" Bolt N	ominal A	rea		=	0.159	)	in <sup>2</sup>	
Shear Stre	ngth per	Bolt		=	3,816	;	lbs	
Tensile Strength per Bolt		=	7,155	<b>;</b>	lbs			
Avail. Tensil	e Streng	th per	Bolt	=	1,781		lbs (Combin	ed Tension and Shear)
Total Bolts Total Bolts	Shear S Tensile	Streng Stren	th gth		$(R_{vb})$ $(R_{tb})$	=	7,632 3,562	lbs lbs
Conclusion								
Shear								
$(V_{EB})$	3,312	lbs	< (R	? <sub>tb</sub> )	7,632	2	lbs	<u>OK</u>
Tension								
(O <sub>EB</sub> )	3,484	lbs	< (F	$(t_{tb})$	3,562	2	lbs	<u>OK</u>

