



ENGINEERING STRUCTURAL CALCULATIONS
For
Gillette 246" Frame Gensets

May 5, 2025

246" LG Frame Genset Models:

SP-6500
SP-8000
PR-5400
PR-6500

Location: Florida

Designed in compliance with: 2023 Florida Building Code, 8th Edition
ASCE 7 - 22 Minimum Design Loads for Buildings and Other Structures
2020 Aluminum Association Design Manual
ANSI/AISC 360-22 - Specification for Structural Steel Buildings

Anchoring: 1/2" Bolt/Anchors - Minimum (6) per side (12) total

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Project Information

Project Name/Model # - Gillette 246" Frame Gensets
Project Number -
 Project Description - Sound Attenuated Generator Enclosure
 Project Location - Florida
 Customer -
 Mounting Location - Ground

Enclosure Materials

Roof Beam - 11 Gauge CRS
 Roof Panels - 14 Ga. CRS
 Wall Panels - 14 Ga. CRS
 Base Frame/Skid - 8 Ga. CRS - Formed C-Channel

Components

GenSet Manufacturer - Gillette
 GenSet Size and Model - SP-6500, SP-8000, PR-5400, PR-6500

Supported by - Base

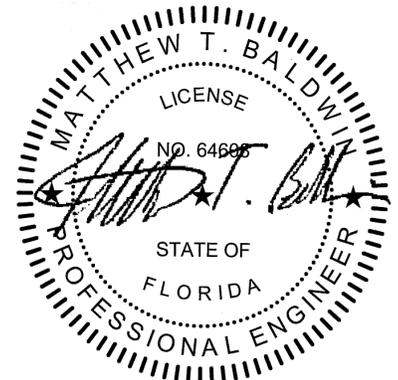
Base - 8 Ga. CRS - Formed C-Channel

Fasteners/Hardware

	Bolt Size	Washer	Nut	Grade/Finish
Roof to Walls	5/16" - 18 Bolts	5/16" Washer	Nut Clip	Grade 18-8/SS
Wall to Wall	5/16" - 18 Bolts	5/16" Washer	Nut Clip	Grade 18-8/SS
Walls to Base	5/16" - 18 Bolts	5/16" Washer	Nut Clip	Grade 18-8/SS
Base to Slab/Tank	1/2" Set Bolt Anchors	Flat Washers	Hex Nuts	Grade 5/Galv.

Specification Requirements

Wind Speed - 200 mph
 Exposure Category - D
 Risk Category - III
 Ground Snow Load (P_g Fig 7.1) - 0 psf
 Ice Thickness (t Fig 10-2 to 10-6) and Concurrent Wind Gust (V_c) - 0.25 in - 30 mph
 Seismic Site Class - B



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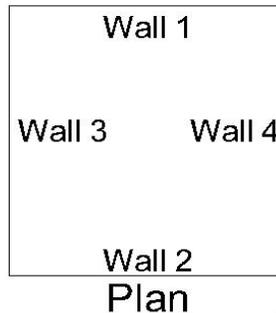
Enclosure Dimensions & Component Weights

Gillette 246" Frame Gensets

Roof Style- Flat

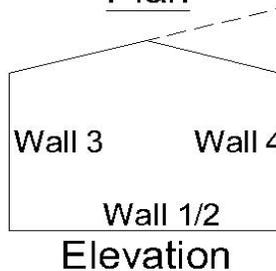
Enclosure Dimensions (ft)

Wall	Length (ft)		Height (ft)
1	7.67	x	8.563
2	7.67	x	8.563
3	20.5	x	8.563
4	20.5	x	8.563



Base Dimensions

Width (Wall 1/2 Side)	=	92	in
Length (Wall 3/4 Side)	=	246	in
Height	=	8	in



Roof/Eave Information

Roof Pitch Angle - (θ)	=	0.0	Degrees
Eave/Roof Height - h	=	9.230	

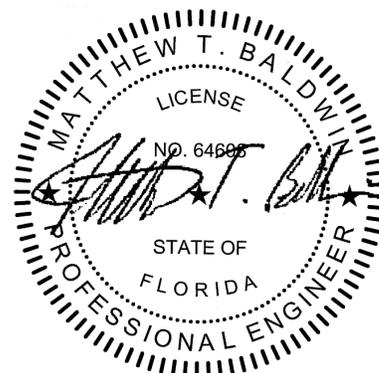
Structure Areas

Walls 1/2 Area - $(w1)$	=	70.8	ft ²	=	10,194	in ²
Walls 3/4 Area - $(w3)$	=	189.2	ft ²	=	27,246	in ²
Roof Area - (R)	=	157.2	ft ²	=	22,642	in ²

Base Side 1/2	$(T1)$	=	736.0	in ²
Base Side 3/4	$(T3)$	=	1,968.0	in ²

Component Weights (lightest setup for worst case)

Genset	=	4,540	lbs
Enclosure	=	11,300	lbs
Base	=	600	lbs



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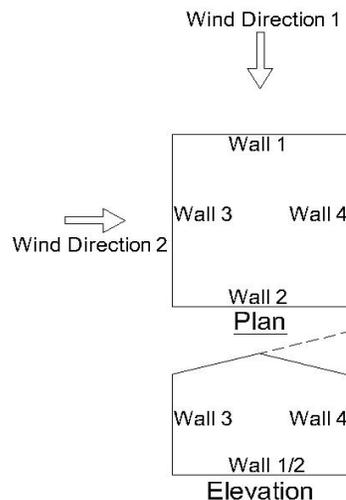
MWFRS Net Pressures

Gillette 246" Frame Gensets

Wind

Analytical Procedure method and Load Combinations from ASCE 7 are utilized in these calculations.

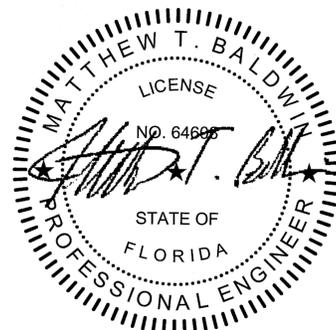
Enclosure Classification	-	Enclosed
Exposure Category	-	D
Basic Wind Speed	(V)	200 mph
Importance Factor (Wind)	(I _w)	1.15
Wind Directionality Factors	(K _d)	0.85
Internal Pressure Coefficients	(GC _{pi})	± 0.18
Velocity Pressure Exposure Coefficient	(K _z)	1.03
Roof Mean Height Above Ground Level	(z)	9.90 ft
Velocity Pressure	(q)	103.12 psf



Wind Direction 1									
	Enclosure								
	Wall #			Roof					
	1	2	3&4	Parallel to Ridge				(C _p)2	
	(C _p)1 (Distance From Windward Edge)								
	Windward	Leeward	Side	0 to 4.6	4.6 to 9.2	9.2 to 18.5	> 18.5		
Background Response Factor (Q)	0.97	0.97	0.95	0.97					
Gust Effect Factors (G)	0.91	0.91	0.90	0.91					
External Pressure Coefficients (C _p)	0.80	-0.266	-0.70	-0.90	-0.90	-0.50	-0.3	-0.18	
Net Pressures with + (GC _{pi}) - psf (Net _{p+})	56.4	-43.5	-83.6	-102.8	-102.8	-65.4	-46.7	-35.4	
Net Pressures with - (GC _{pi}) - psf (Net _{p-})	93.5	-6.4	-46.5	-65.7	-65.7	-28.3	-9.5	1.7	

Wind Direction 2									
	Enclosure								
	Wall #			Roof - Normal To Ridge					
	3	4	1&2	(C _p)1 (Distance From Windward Edge)				(C _p)2	
	(C _p)1 (Distance From Windward Edge)								
	Windward	Leeward	Side	0 to 4.6	> 4.6				
Background Response Factor (Q)	0.95	0.95	0.97	0.95					
Gust Effect Factors (G)	0.90	0.90	0.91	0.90					
External Pressure Coefficients (C _p)	0.80	-0.5	-0.70	-1.04	-0.70			-0.18	
Net Pressures with + (GC _{pi}) - psf (Net _{p+})	55.8	-65.0	-84.1	-115.2	-83.6			-35.3	
Net Pressures with - (GC _{pi}) - psf (Net _{p-})	92.9	-27.9	-47.0	-78.1	-46.5			1.8	

Plus and minus signs signify pressures acting toward or away from the surfaces, respectively.



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Snow

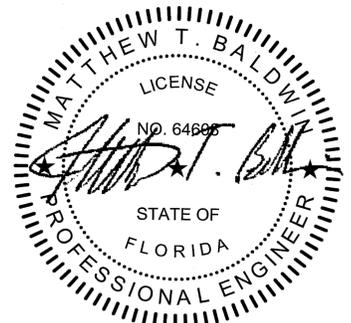
Importance Factor (Snow)	(I_s)	1.1	
Exposure Factor	(C_e)	0.8	
Thermal Factor	(C_t)	1.2	
Slope Factor	(C_s)	1.0	
Flat Roof Snow Load	(p_s)	0	psf

Seismic

Importance Factor (Seismic)	(I_{sm})	1.25	
Mapped Acceleration Parameter	(S_s)	0.14	Figures 22-1 Thru 22-14
Mapped Acceleration Parameter	(S_1)	0.07	Figures 22-1 Thru 22-14
Site Coefficient	(F_a)	1	
Site Coefficient	(F_v)	1	
MCE Spectral Resp. Accel. Short Per.	(S_{MS})	0.140	
MCE Spectral Resp. Accel. 1-s Period	(S_{M1})	0.07	
Design Spectral Accel. Short Period	(S_{DS})	0.093	
Design Spectral Accel. 1-s Period	(S_{D1})	0.04667	
Fundamental Period of Structure	(T_a)	0.100	sec
Long Period Transition Period	(T_L)	8	sec Figure 22-15 Thru 22-20
Seismic Design Category	-	A	
Total Effective Seismic Weight	(W_{eff})	19,708	lbs
Response Modification Coefficient	(R)	2	Table 12.2-1
System Overstrength Factor	(Ω_o)	2.5	Table 12.2-1
Deflection Amplification Factor	(C_d)	2	Table 12.2-1
Seismic Response Coefficient	(C_s)	0.058	

Resultant Seismic Forces

Horizontal Seismic Load Effect	-	(E_h)	
Force at Base of Base	=	0.2	kips
Force at Top of Base	=	0.2	kips
Force at Top/Bottom of Enclosure	=	0.113	kips
Force on Silencer	=	0	kips
Vertical Seismic Load Effect (E_v)	=	0	(Factor, Used With Deadweight in Load Combinations)



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Structural Calculations - Roof

Gillette 246" Frame Gensets

Critical Loads & Pressures

Wind Pressures

Downforce 1.829 psf = 0.01 psi
Uplift -115.2 psf = -0.80 psi

Snow Pressure

0 psf = 0.000 psi

Seismic Load

Horizontal = 113 lbs
Vertical Factor = 0

Roof Live Load

Downforce 20.0 psf = 0.1389 psi or 300 lbs Concentrated Load

Pressures & loads are the numerical maximums to be analyzed for shear, bending tension, and compression.

Section Properties

11 Gauge CRS

Cross Sectional Area (A) = 1.88 in²
Moment of Inertia - x (I_x) = 2.800 in⁴
Moment of Inertia - y (I_y) = N/A in⁴
Section Modulus - x (S_x) = 2.130 in³
Section Modulus - y (S_y) = N/A in³
Radius of Gyration - x (r_x) = 1.220 in
Radius of Gyration - y (r_y) = N/A in

Weight (ω) = 0.470 lbs/in
Modulus of Elasticity (E) = 2.90E+04 ksi
Safety Factor (Ω) = 1.95
Plastic Section Mod. - x (Z_x) = 0.24
Plastic Section Mod. - y (Z_y) = 0.24
Tensile Ultimate Strength (F_{tu}) = 58 ksi
Tensile Yield Strength (F_{ty}) = 36 ksi
Compressive Yield Strength (F_{cy}) = 22 ksi
Shear Ultimate Strength (F_{su}) = 36 ksi

Roof Frame Calculations

Member Designed for Forces Acting on the **Strong Axis**

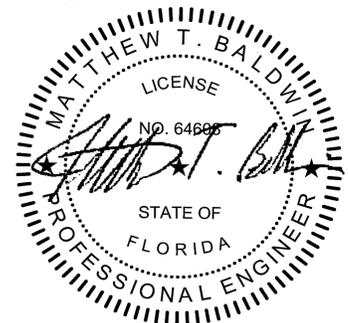
Interior Beam Critical Member Dimensions

Interior Beam Length (L_i) = 91.8 in
Load Spanned Width (W_i) = 32 in

Interior Beam Calculated Forces

Distributed Loads

Weight of Beam (ω) = 0.029 lbs/in
Wind Load Downforce (W_d) = 0.407 lbs/in
Wind Load Uplift Force (W_u) = -25.609 lbs/in



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Shear Forces (Maximum at End)

Beam Weight Shear (V_b) = 1.75 lbs
Wind DownForce Shear (V_{wd}) = 9.7 lbs
Wind Uplift Shear (V_{wu}) = -664.3 lbs
Total Shear Downward = 11.5 lbs
Total Shear Upward = 662.5 lbs
Design Shear (V_{bi}) = 662.5 lbs

Stress Forces (Bending)

Beam Weight Moment (M_b) = 11 lb-in
Wind Downforce Moment (M_d) = 47 lb-in
Wind Uplift Moment (M_u) = -3,223 lb-in
Total Moments Downward = 59 lb-in
Total Moments Upward = 3,211 lb-in
Design Moment (M_T) = 3,211 lb-in
Design Stress (σ_{bi}) = 8,921 psi

Interior Beam Design Calculations

Allowable Shear Strength

Slenderness Limit 1 (S_1) = -20.08
Slenderness Limit 2 (S_2) = 102.40
Slenderness Ratio (S) = 18.0
Allowable Shear Stress = 9,856 psi
Allowable Shear Strength (V_n) = 3,548 lbs

Conclusion

(V_{bi}) 663 lbs < (V_n) 3,548 lbs **OK**

Allowable Stresses For Tension And Compression (Bending)

Tension

Allowable Tensile Stress (F_t) = 90,240 psi

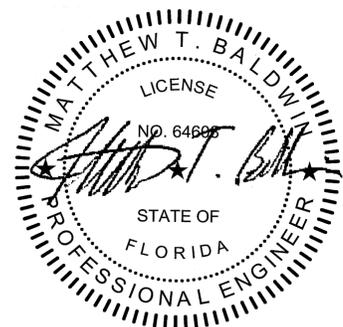
Compression

Slenderness Limit 1 (S_1) = 25.0
Slenderness Limit 2 (S_2) = 125.0
Slenderness Ratio (S) = 41.3
Allowable Compressive Stress (F_c) = 13,121 psi

The Allowable Compressive Stress is the controlling failure design
Therefore, (F_b) = 13,121 psi

Conclusion

(σ_{bi}) 8,921 psi < (F_b) 13,121 psi **OK**



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Entire Roof Uplift Calculations

Roof Area

Area of Roof Subjected to Uplift $(R) = 22,642 \text{ in}^2$ (not including discharge hood area)

Roof Uplift Calculated Forces

Roof Weight $(\omega_a) = 102 \text{ lbs}$

Wind Load Uplift Force $(W_{ru}) = -18,120 \text{ lbs}$

Total Roof Design Uplift $(W_{ru}) = -18,018 \text{ lbs}$

Mounting Hardware - Roof Frame to Wall Panels

Screws Along Length - 1 Side = 17 5/16" - 18 Bolts

Screws Along Width - 1 Side = 6 5/16" - 18 Bolts

Total Mounting Screws = 46 5/16" - 18 Bolts

Entire Roof Uplift Design Calculations

Grade 18-8/SS Ult. Strength = 150,000 psi

5/16" Bolt Nominal Diameter = 0.255 in

5/16" Bolt Effective Area = 0.051 in²

5/16" Bolt Threads per Inch = 18

Washer Nominal Diameter = 0.875 in

Wall Panel Tensile Ult. Strength = 58 ksi

Wall Panel Tensile Yield Strength = 36 ksi

Safety Factor = 3

Wall Panel Nominal Thickness = 0.0780 in

Maximum Tensile Strength = 942.5 lbs

Maximum Shear/Bearing Strength = 408.6 lbs

Max. Tensile Load per Bolt = 408.6 lbs

Max. Total Screws Tensile Strength $(P_{ts}) = 18,794 \text{ lbs}$

Conclusion

$(W_{ru}) \quad 18,018 \text{ lbs} < (P_{ts}) \quad 18,794 \text{ lbs} \quad \text{OK}$

Roof Panel Uplift Calculations

Roof Panel Critical Member Dimensions

Critical Panel Length $(L_p) = 64.00 \text{ in}$

Critical Panel Width $(W_p) = 92.00 \text{ in}$

Roof Panel Uplift Calculated Forces

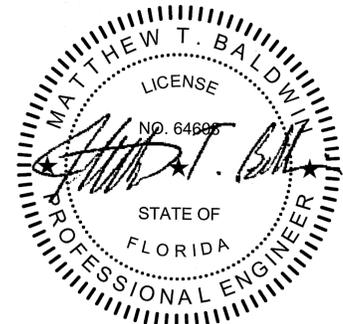
Distributed Loads

Wind Load Uplift Force $(W_{pu}) = 4,712.0 \text{ lbs}$

Mounting Hardware - Roof Panel to Roof Frame

Screws Along Length - 1 Side = 6 5/16" - 18 Bolts - Grade 18-8/SS

Screws Along Width - 1 Side = 2 5/16" - 18 Bolts - Grade 18-8/SS



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Roof Panel Uplift Design Calculations

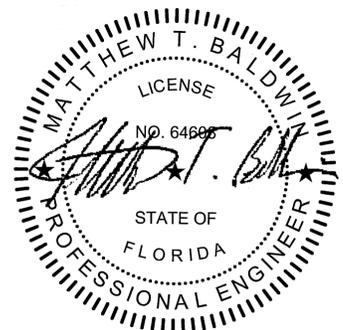
Grade 18-8/SS Ult. Strength = 150,000 psi
5/16" Bolt Nominal Diameter = 0.255 in
5/16" Bolt Effective Area = 0.051 in²
5/16" Bolt Threads per Inch = 18
Washer Nominal Diameter = 0.875 in
Roof Panel Tensile Ult. Strength = 34 ksi
Roof Panel Tensile Yield Strength = 26 ksi
Safety Factor = 3
Roof Panel Nominal Thickness = 0.0800 in

	Roof Frame	
Maximum Tensile Strength =	552.5	(Accounts for screw pull-over and pull-out strengths)
Maximum Shear/Bearing Strength =	408.6	
Max. Tensile Load per Screw =	408.6	

Max. Total Screws Tensile Strength (P_{ts}) = 6,537 lbs

Conclusion

(w_{pu}) 4,712 lbs < (P_{ts}) 6,537 lbs **OK**



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Structural Calculations - Wall Panel

Gillette 246" Frame Gensets

Critical Loads & Pressures

Walls 1 & 2

Maximum Pressures Acting:

$$\begin{aligned} \text{Toward} & 93.5 \text{ psf} = 0.6492 \text{ psi} \\ \text{Away} & -84.1 \text{ psf} = -0.5841 \text{ psi} \end{aligned}$$

Walls 3 & 4

Maximum Pressures Acting:

$$\begin{aligned} \text{Toward} & 92.9 \text{ psf} = 0.6453 \text{ psi} \\ \text{Away} & -83.6 \text{ psf} = -0.5808 \text{ psi} \end{aligned}$$

Roof Forces on Critical Panel (From Roof Frame Calculations)

$$\begin{aligned} \text{Maximum Downforce} & (W_d) = 3,247 \text{ lbs} \\ \text{Wind Load Uplift Force} & (W_{pu}) = 4,712 \text{ lbs} \end{aligned}$$

Pressures and weights are the numerical maximums to be analyzed for shear, tension, and compression.

Critical Wall Panel Dimensions

$$\begin{aligned} \text{Critical/Maximum Panel Width} & = 60.00 \text{ in} \\ \text{Critical/Maximum Panel Height} & = 108.50 \text{ in} \end{aligned}$$

Section Properties

14 Ga. CRS

$$\begin{aligned} \text{Cross Sectional Area} & (A) = 5.08 \text{ in}^2 \\ \text{Moment of Inertia - x} & (I_x) = 2.340 \text{ in}^4 \\ \text{Moment of Inertia - y} & (I_y) = \text{N/A} \text{ in}^4 \\ \text{Section Modulus - x} & (S_x) = 9.310 \text{ in}^3 \\ \text{Section Modulus - y} & (S_y) = \text{N/A} \text{ in}^3 \\ \text{Radius of Gyration - x} & (r_x) = 0.680 \text{ in} \\ \text{Radius of Gyration - y} & (r_y) = \text{N/a} \text{ in} \\ \text{Weight} & (w) = 0.117 \text{ lbs/in}^2 \\ \text{Modulus of Elasticity} & (E) = 2.90\text{E}+04 \text{ ksi} \\ \text{Safety Factor} & (\Omega) = 1.67 \\ \text{Plastic Section Mod. - x} & (Z_x) = 0.24 \\ \text{Plastic Section Mod. - y} & (Z_y) = 0.24 \\ \text{Tensile Ultimate Strength} & (F_{tu}) = 58 \text{ ksi} \\ \text{Tensile Yield Strength} & (F_{ty}) = 36 \text{ ksi} \\ \text{Compressive Yield Strength} & (F_{cy}) = 22 \text{ ksi} \\ \text{Shear Ultimate Strength} & (F_{su}) = 12 \text{ ksi} \end{aligned}$$

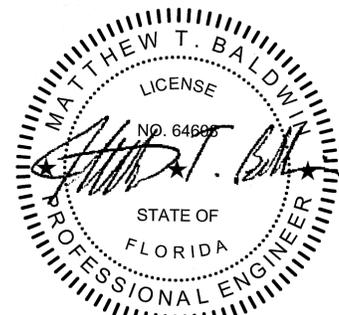
Wall Panel Calculations

Critical Wall Area

$$\text{Area of Wall Panel} (W) = 6,510.0 \text{ in}^2$$

Mounting Hardware - Roof Frame to Wall Panels

$$\begin{aligned} \text{Screws Along Height - 1 Side} & = 3 & 5/16" - 18 \text{ Bolts} \\ \text{Screws Along Width - 1 Side} & = 3 & 5/16" - 18 \text{ Bolts} \\ \text{Total Mounting Screws} & = 12 & 5/16" - 18 \text{ Bolts} \end{aligned}$$



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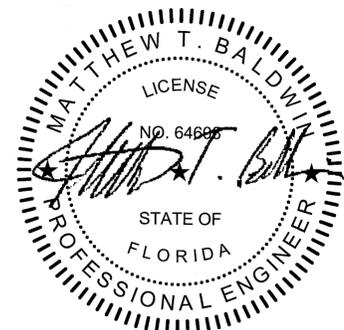
Grade 5 Ultimate Strength = 150,000 psi
 5/16" Bolt Nominal Diameter = 0.255 in
 5/16" Bolt Effective Area = 0.051 in²
 5/16" Bolt Threads per Inch = 18
 Washer Nominal Diameter = 0.875 in
 Roof Panel Tensile Ult. Strength = 58 ksi
 Roof Panel Tensile Yield Strength = 36 ksi
 Safety Factor = 1.65
 Roof Panel Nominal Thickness = 0.0800 in

	Roof Frame	
Maximum Tensile Strength	= 1054.9	(Accounts for screw pull-over and pull-out strengths)
Maximum Shear/Bearing Strength	= 300.0	
Max. Tensile Load per Bolt	= 300.0	

Max. Total Screws Tensile Strength (P_{ts}) = 4,804 lbs

Conclusion

(W_{pu}) 4,226 lbs < (P_{ts}) 4,804 lbs **OK**



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Structural Calculations - Enclosure to Base

Gillette 246" Frame Gensets

Critical Pressures & Loads

To determine maximum moment forces, pressures are algebraically combined relative to toward or away forces (+ & -) and each wind direction.

Wind Direction 1

To be conservative, roof downforce is neglected.

Net Pressures with + Internal Pressure(+Gcpi)

Walls 1 & 2	-	99.9	psf =	0.6935	psi
Wall 3 or 4	-	83.6	psf =	0.5808	psi
Roof Uplift	-	102.8	psf =	0.7142	psi

Net Pressures with - Internal Pressure(-Gcpi)

Walls 1 & 2	-	99.9	psf =	0.6935	psi
Wall 3 or 4	-	46.5	psf =	0.3230	psi
Roof Uplift	-	65.7	psf =	0.4564	psi

Wind Direction 2

Net Pressures with + Internal Pressure(+Gcpi)

Walls 3 & 4	-	120.8	psf =	0.8392	psi
Wall 1 or 2	-	84.1	psf =	0.5841	psi
Roof Uplift	-	115.2	psf =	0.8003	psi

Net Pressures with - Internal Pressure(-Gcpi)

Walls 3 & 4	-	120.8	psf =	0.8392	psi
Wall 1 or 2	-	47.0	psf =	0.3263	psi
Roof Uplift	-	78.1	psf =	0.5425	psi

Seismic

Horizontal Seismic Force (E_h) = 113 lbs

Enclosure Critical Dimensions & Weights

Total Enclosure Weight (W _t)	=	15,840.0	lbs	(Includes all components)
Walls 1/2 Area	-	(w1)	= 10194.0	in ²
Walls 3/4 Area	-	(w3)	= 27246.0	in ²
Roof Area	-	(R)	= 22641.8	in ²

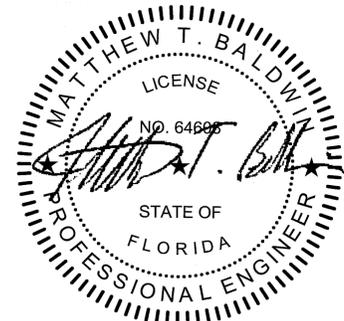
Enclosure Calculated Forces

Maximum Wind Load Forces on Walls

Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Walls 1/2	-	=	7,069	lbs
Wall 3 or 4	-	=	15,824	lbs
Roof Uplift	-	=	16,171	lbs



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Net Forces with - Internal Pressure(-Gcpi)

Walls 1/2	-	=	7,069	lbs
Wall 3 or 4	-	=	8,800	lbs
Roof Uplift	-	=	10,334	lbs

Wind Direction 2

Net Forces with + Internal Pressure(+Gcpi)

Walls 3/4	-	=	22,865	lbs
Wall 1 or 2	-	=	5,955	lbs
Roof Uplift	-	=	18,120	lbs

Net Forces with - Internal Pressure(-Gcpi)

Walls 3/4	-	=	22,865	lbs
Wall 1 or 2	-	=	3,327	lbs
Roof Uplift	-	=	12,282	lbs

Enclosure Overturn Forces (Includes Seismic)

(Postive forces act upward, negative forces act downward)

Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 1/2	=	1,757	lbs
Overturn on Walls 3/4	=	9,686	lbs

Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 1/2	=	-1,162	lbs
Overturn on Walls 3/4	=	2,542	lbs

Wind Direction 2

Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 3/4	=	14,897	lbs
Overturn on Walls 1/2	=	2,480	lbs

Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 3/4	=	11,978	lbs
Overturn on Walls 1/2	=	-1,030	lbs

Design Overturn Force (O_E) = 14,897 lbs Acting On Wall 3/4

Mounting Hardware - Enclosure to Base/Tank or Pad

To be conservative, bolt connections along the adjacent walls are neglected.

No. of Bolt Connections Along Wall 3/4 = 11 5/16" - 18 Bolts - Grade 18-8/S

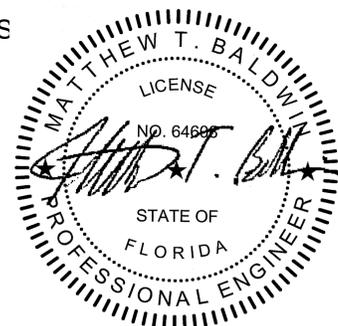
Enclosure Overturn Design Calculations

Grade 18-8 Ultimate Strength	=	150,000	psi
Grade 8.8 Nom. Tensile Stress	=	112,500	psi (Includes Reduction Factor)
5/16" Bolt Effective Area	=	0.051	in ²
Tensile Strength per Bolt	=	2,873	lbs

Total Bolts Tensile Strength = 31,600 lbs

Conclusion

(O_E) 14,897 lbs < (R_v) 31,600 lbs **OK**



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Structural Calculations - Enclosure With Base/Tank to Pad

Gillette 246" Frame Gensets

Critical Wind Load Pressures

To determine maximum moment forces, pressures are algebraically combined relative to toward or away forces (+ & -) and each wind direction.

Wind Direction 1

To be conservative, roof downforce is neglected.

Net Pressures with + Internal Pressure(+Gcpi)

Walls 1 & 2	-	99.9	psf =	0.6935	psi
Wall 3 or 4	-	83.6	psf =	0.5808	psi
Roof Uplift	-	102.8	psf =	0.7142	psi

Net Pressures with - Internal Pressure(-Gcpi)

Walls 1 & 2	-	99.9	psf =	0.6935	psi
Wall 3 or 4	-	46.5	psf =	0.3230	psi
Roof Uplift	-	65.7	psf =	0.4564	psi

Wind Direction 2

Net Pressures with + Internal Pressure(+Gcpi)

Walls 3 & 4	-	120.8	psf =	0.8392	psi
Wall 1 or 2	-	84.1	psf =	0.5841	psi
Roof Uplift	-	115.2	psf =	0.8003	psi

Net Pressures with - Internal Pressure(-Gcpi)

Walls 3 & 4	-	120.8	psf =	0.8392	psi
Wall 1 or 2	-	47.0	psf =	0.3263	psi
Roof Uplift	-	78.1	psf =	0.5425	psi

Seismic

Enclosure Horiz. Seismic Force (EE_h) = 113 lbs

Base/Tank Horiz. Seismic Force (EB_h) = 197 lbs

Enclosure With Base/Tank Critical Dimensions & Weights

Total Enclosure Weight	(W _t)	=	16,440	lbs	(Includes all components)
Walls 1/2 Area	-	(w1)	=	10,930	in ² (Includes Base/Tank Surface Area)
Walls 3/4 Area	-	(w3)	=	29,214	in ² (Includes Base/Tank Surface Area)
Roof Area	-	(R)	=	22,642	in ²

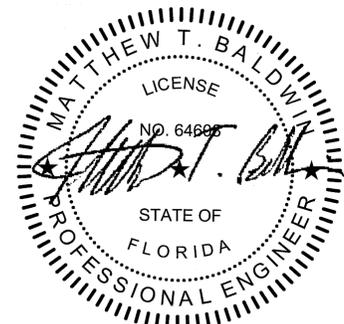
Enclosure With Base/Tank Calculated Forces

Maximum Wind Shear Forces on Walls Including Base/Tank

Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Walls 1/2	-	=	7,580	lbs
Wall 3 or 4	-	=	16,967	lbs
Roof Uplift	-	=	16,171	lbs



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Net Forces with - Internal Pressure(-Gcpi)

Walls 1/2	-	=	7,580	lbs
Wall 3 or 4	-	=	9,436	lbs
Roof Uplift	-	=	10,334	lbs

Wind Direction 2

Net Forces with + Internal Pressure(+Gcpi)

Walls 3/4	-	=	24,517	lbs
Wall 1 or 2	-	=	6,385	lbs
Roof Uplift	-	=	18,120	lbs

Net Forces with - Internal Pressure(-Gcpi)

Walls 3/4	-	=	24,517	lbs
Wall 1 or 2	-	=	3,567	lbs
Roof Uplift	-	=	12,282	lbs

Enclosure with Base/Tank Maximum Wind Force = 24,517 lbs Acting On Wall 3/4

Coefficient of Friction - Steel to Wet Concrete (μ_s) = 0.45

Frictional Resisting Force (Total Weight x μ_s) = 7,398

Enclosure with Base/Tank Design Shear (V_{EB}) = 17,119

Enclosure With Base/Tank Overturn Forces (Inlcudes Seismic)

Postive forces act upward

Wind Direction 1

Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 1/2	=	1,756	lbs
Overturn on Walls 3/4	=	10,974	lbs

Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 1/2	=	-1,163	lbs
Overturn on Walls 3/4	=	3,197	lbs

Wind Direction 2

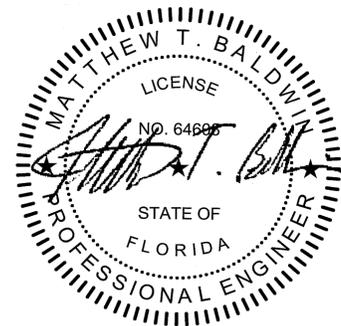
Net Forces with + Internal Pressure(+Gcpi)

Overturn on Walls 3/4	=	16,819	lbs
Overturn on Walls 1/2	=	2,442	lbs

Net Forces with - Internal Pressure(-Gcpi)

Overturn on Walls 3/4	=	13,901	lbs
Overturn on Walls 1/2	=	-1,157	lbs

Design Overturn Force (O_{EB}) = 16.819 lbs Acting On Wall 3/4



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Mounting Hardware - Enclosure With Base/Tank to Pad

No. of Bolt Connections Along Wall 3/4 = 6 Bolts 1/2" Set Bolt Anchors - Grade 5/Galv.

Enclosure With Base/Tank Design Calculations

Mounting Hardware - Shear and Tension

Grade 5 Ultimate Stress = 120,000 psi
Grade 5 Nom. Shear Stress = 48,000 psi
Grade 5 Nom. Tensile Stress = 90,000 psi
1/2" Bolt Nominal Area = 0.159 in²
Shear Strength per Bolt = 3,816 lbs
Tensile Strength per Bolt = 7,155 lbs
Avail. Tensile Strength per Bolt = 2,862 lbs (Combined Tension and Shear)

Total Bolts Shear Strength (R_{vb}) = 22,896 lbs
Total Bolts Tensile Strength (R_{tb}) = 17,172 lbs

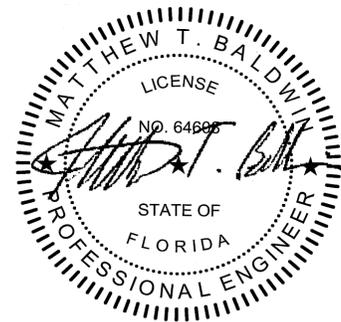
Conclusion

Shear

(V_{EB}) 17,119 lbs < (R_{tb}) 22,896 lbs **OK**

Tension

(O_{EB}) 16,819 lbs < (R_{tb}) 17,172 lbs **OK**



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